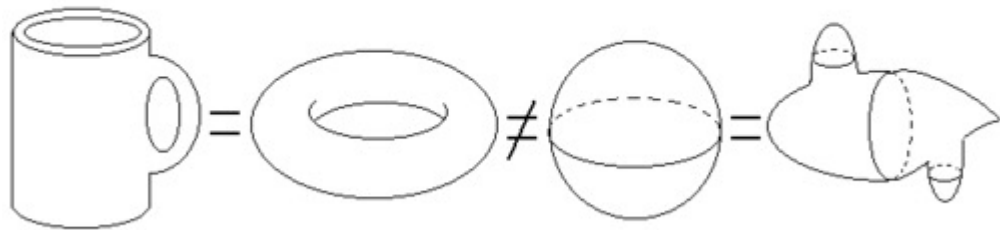
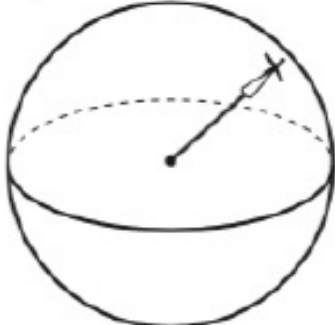
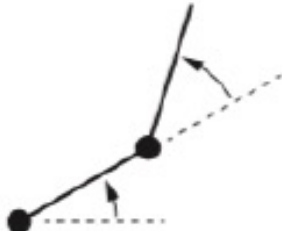
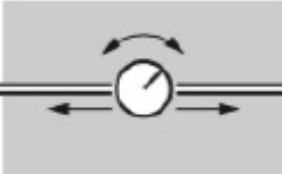


Configuration Space: Topology

- If $\text{dof} = n$, then is the C-space is $\mathbb{R}^n$?
 - No! Spaces can have different shapes or **topologies**
- A circle is written as a S or S^1
- A line can be written as $\mathbb{E}$ or $\mathbb{E}^1$ or $\mathbb{R}$
- A choice of n coordinates to represent an n -dimensional space is called an **explicit parametrization**.



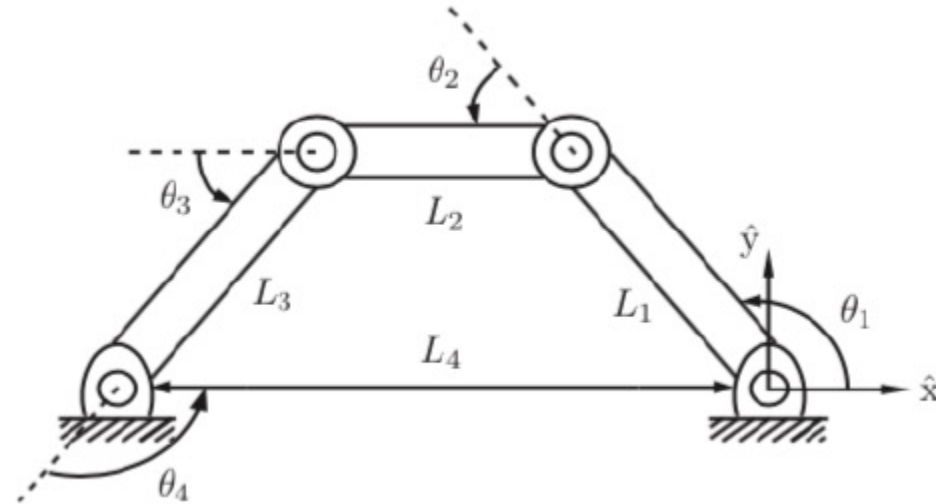
system	topology
	 $\mathbb{E}^2$
	 S^2
	 $T^2 = S^1 \times S^1$
	 $\mathbb{E}^1 \times S^1$

Configuration Space Representation

- An **implicit representation** is given by constrained coordinates
- It is often easier to obtain than an **explicit representation**
 - For instance, instead of a spherical representation, we can use a higher dimensional space like (x, y, z) and subject it to constraints to reduce the DoF ($x^2 + y^2 + z^2 = 1$)

Configurations and Constraints

How many DoF?



$$L_1 \cos \theta_1 + L_2 \cos(\theta_1 + \theta_2) + \cdots + L_4 \cos(\theta_1 + \cdots + \theta_4) = 0$$

$$L_1 \sin \theta_1 + L_2 \sin(\theta_1 + \theta_2) + \cdots + L_4 \sin(\theta_1 + \cdots + \theta_4) = 0$$

$$\theta_1 + \theta_2 + \theta_3 + \theta_4 - 2\pi = 0$$

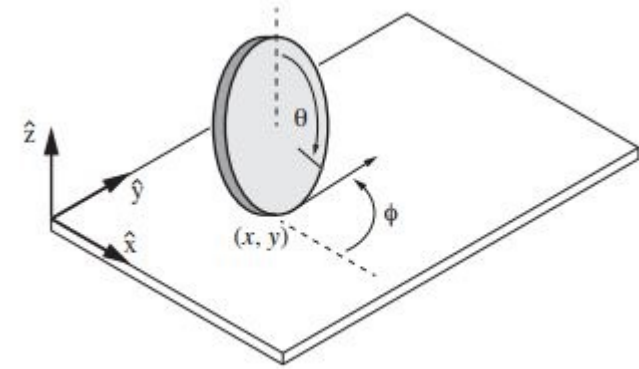
Types of Constraints

Holonomic constraints decrease the dimension of the C-space, while **non-holonomic** constraints do not.

Types of Constraints

- Suppose we are given Pfaffian constraints $A(\theta)\dot{\theta} = 0$
- If we can find a function g such that $\frac{\partial g}{\partial \theta} = A$, the (integrable) constraints g are **holonomic**
 - Why? If such g exists, the constraints $A(\theta)\dot{\theta} = 0$ are the same as the constraints on the position variables $g(\theta)$
- If no such g exists, the constraints are called **non-holonomic**

Rolling Penny Example



Summary

- Introduced fundamental robotics definitions like **configuration space**, **task space**, and **workspace**
- Learned methods for determining the number of **degrees of freedom** for a rigid body and robot mechanism
- Discussed **holonomic and non-holonomic constraints** which may affect the configuration space and mobility of a robot



Credit: Wikipedia

1.
2.

ECEB 2036 3-5 PM

HW1 is due at 11.59 PM on Fri.

Who was Benjamin Olinde Rodrigues?

Charles

- A mathematician who turned to finance for employment
 - PhD in math and became a banker
- His dissertation introduced the Rodrigues formula
 - Formerly known as the Ivory–Jacobi formula, as it was independently introduced by Olinde Rodrigues (1816), Sir James Ivory (1824), and **Carl Gustav Jacobi (1827)**

→ Exponential coordinates for rotation

Types of Constraints

Constraints : remove DOFs.

general rule : 1 constraint removes 1 DOF.

- It can be broken in several ways.
 - Constraints can be dependent $\leadsto$ does not remove a DOF.

θ_1, θ_2

$$\begin{cases} q_1(\theta_1, \theta_2) = \theta_1 + \theta_2 - 1 = 0 \\ q_2(\theta_1, \theta_2) = (\theta_1 + \theta_2 - 1)^2 = 0 \end{cases}$$

↳ a colian test for constraints
in dependence.

$\frac{\partial g}{\partial \theta}$ is full rank if constraints are $\frac{11}{\downarrow}$
indep.

$$\begin{bmatrix} \frac{\partial g_1}{\partial \theta_1} & \frac{\partial g_1}{\partial \theta_2} \\ \frac{\partial g_2}{\partial \theta_1} & \frac{\partial g_2}{\partial \theta_2} \end{bmatrix} = \begin{bmatrix} 1 & 1 \\ (\theta_1 + \theta_2 - 1) & (\theta_1 + \theta_2 - 1) \end{bmatrix}$$

↳ rank 1 $\Rightarrow$ constraints
are dependent $\begin{cases} \text{row 2} = \\ \text{row 1} \cdot (\theta_1 + \theta_2 - 1) \end{cases}$

$$\cdot \quad \theta_1^2 + \theta_2^2 = 0$$

1 constraint removed 2 DOF!

↳ singularity [won't look at this]

Rolling Penny Example

4 DOF (x, y, ϕ, θ)

$$\dot{\mathbf{x}} = \frac{d}{dt} \mathbf{x}$$

$$\dot{\theta} = \frac{d}{dt} \theta$$

$$\begin{aligned} \dot{x} &= r \dot{\theta} \cos \phi \Leftrightarrow \dot{x} - r \cos \phi \dot{\theta} = 0 \\ \dot{y} &= r \dot{\theta} \sin \phi \Leftrightarrow \dot{y} - r \sin \phi \dot{\theta} = 0 \end{aligned}$$

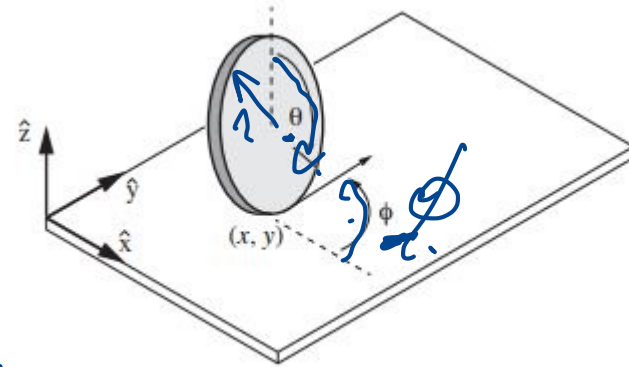
Proffian form: $A(\theta) \dot{\theta} = 0$

$\theta = [x, y, \phi, \dot{\theta}]$: if $g \exists$, then

cohomology

$$\frac{\partial g_1}{\partial \theta_1} = 1 \quad \frac{\partial g_2}{\partial \theta_1}$$

$$A(\theta) = \begin{bmatrix} 1 & 0 & 0 & -r \cos \phi \\ 0 & 1 & 0 & -r \sin \phi \end{bmatrix} \begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{\phi} \\ \dot{\theta} \end{bmatrix} = 0$$



$$\begin{aligned} \dot{x} &= r \dot{\theta} \cos \phi \\ \dot{y} &= r \dot{\theta} \sin \phi \end{aligned}$$

Q: $\exists ? g$ s.t

$$\frac{\partial g}{\partial \theta} = A ?$$

$$\begin{bmatrix} 1 & 0 & 0 & -r c_\phi \\ 0 & 1 & 0 & -r s_\phi \end{bmatrix}$$

$\leadsto$ If $g = \begin{bmatrix} g_1 \\ g_2 \end{bmatrix} \in \mathbb{R}^2$, then

$$\frac{\partial g_1}{\partial x} = 1$$

$$\frac{\partial g_1}{\partial y} = 0$$

$$\frac{\partial g_1}{\partial \phi} = 0$$

$$\frac{\partial g_2}{\partial \phi} = -r c_\phi$$

this implies that

$$\frac{\partial^2 g_1}{\partial \phi \partial \phi} = r s_\phi \neq \frac{\partial^2 g_1}{\partial \phi \partial \phi} = 0.$$

$\leadsto$ Contradiction: g does not exist.

$\Rightarrow$ Constraint is non-holonomic.

Example: $\dot{\theta}_1 \theta_1 + \dot{\theta}_2 \theta_2 = 0$

$$A(\theta) \leftarrow \begin{matrix} \begin{matrix} \theta_1 & \theta_2 \end{matrix} \\ \begin{matrix} \frac{\partial g_1}{\partial \theta_1} & \frac{\partial g_1}{\partial \theta_2} \end{matrix} \end{matrix} \begin{bmatrix} \dot{\theta}_1 \\ \dot{\theta}_2 \end{bmatrix}$$

$$\frac{\partial^2 g_1}{\partial \theta_1 \partial \theta_2} = 0 \neq \frac{\partial^2 g_1}{\partial \theta_2 \partial \theta_1} \quad \checkmark \quad \text{Cannot Conclude}$$

$$g = \frac{\theta_1^2}{2} + \frac{\theta_2^2}{2} \quad \sim \text{holonomic.}$$

$$\underline{ex:} = \frac{\dot{\theta}_1 \theta_2 - \dot{\theta}_2 \theta_1}{\theta_1^2 + \theta_2^2} = 0.$$

Summary

- Introduced fundamental robotics definitions like **configuration space**, **task space**, and **workspace**
- Learned methods for determining the number of **degrees of freedom** for a rigid body and robot mechanism
- Discussed **holonomic and non-holonomic constraints** which may affect the configuration space and mobility of a robot

Rigid Body Motions

Frames of Reference

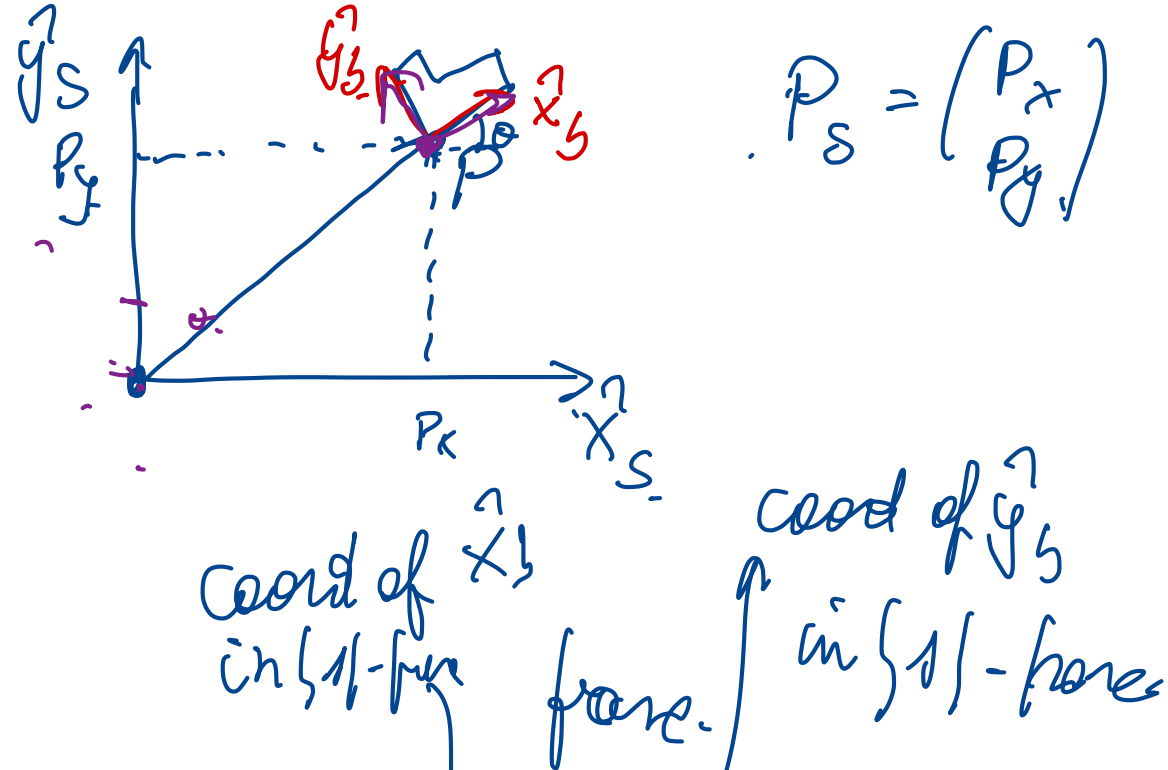
$\{1\}$ - frame.
 $\hat{x}$ means it is normalized.

$\hat{x}_b \sim$ body.

$\{P_S, \hat{x}_b, \hat{y}_b\}$ is called a frame!

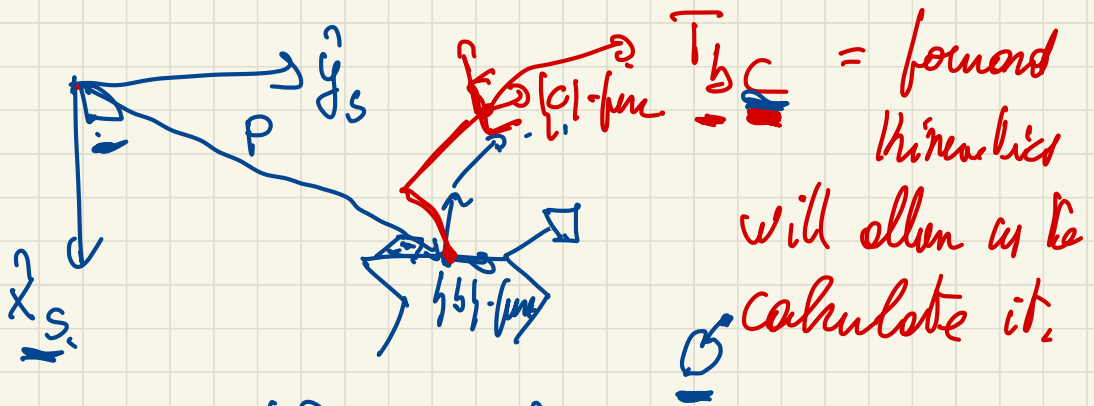
$$P = P_x \hat{x}_S + P_y \hat{y}_S$$

$$\hat{x}_b = \begin{pmatrix} c_\theta \\ s_\theta \end{pmatrix} \quad \hat{y}_b = \begin{pmatrix} -s_\theta \\ c_\theta \end{pmatrix}$$



$$T_{Sb} = \begin{bmatrix} c_\theta & -s_\theta & P_x \\ s_\theta & c_\theta & P_y \\ 0 & 0 & 1 \end{bmatrix}$$

$R_{Sb} =$ rotation matrix.



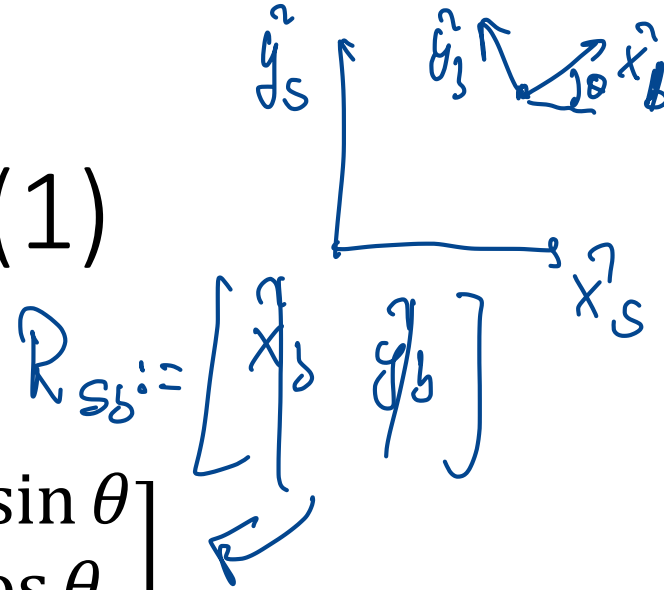
$$T_{sb} = \begin{pmatrix} R_{sb} & P \\ 0 & 1 \end{pmatrix}$$

$$T_{sb} T_{bc} = T_{sc}$$

Rotation Matrices (1)

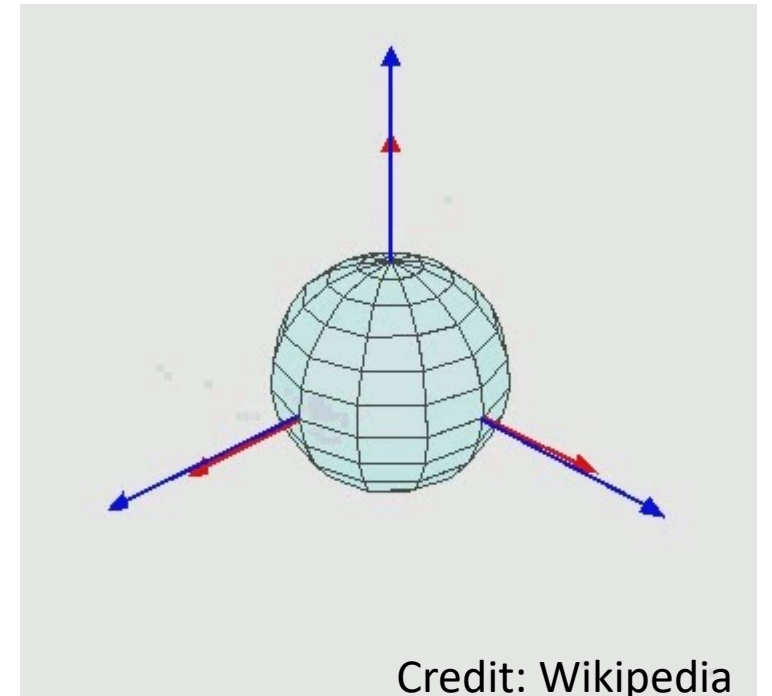
- 2D rotations:

$$\underline{R(\theta)} = \begin{bmatrix} \cos \theta & -\sin \theta \\ \sin \theta & \cos \theta \end{bmatrix}$$

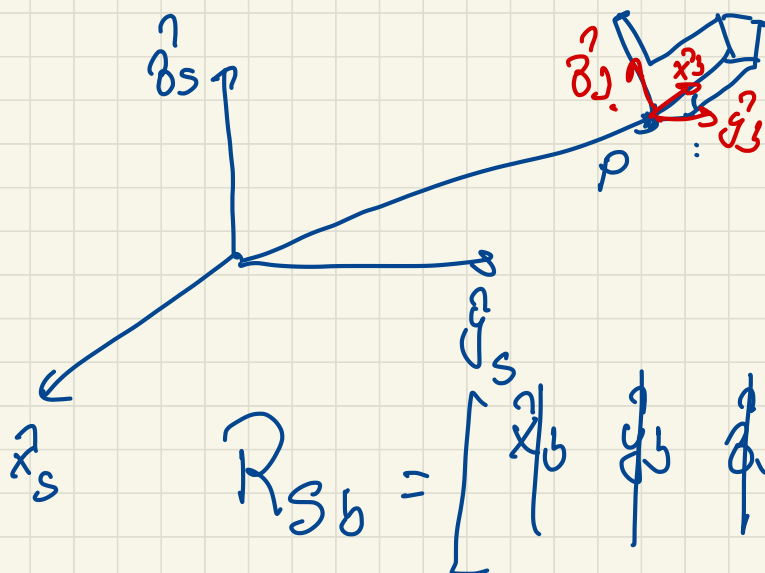


- 3D rotations about a main axis:

$$R_x(\theta) = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos \theta & -\sin \theta \\ 0 & \sin \theta & \cos \theta \end{bmatrix}$$



Credit: Wikipedia

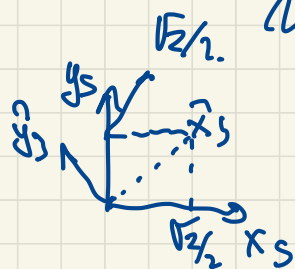


$$R_{sb} = \begin{bmatrix} | & | & | \\ x_b & y_b & z_b \\ | & | & | \end{bmatrix}$$

$$T_{sb} = \begin{bmatrix} \underline{R_{sb}} & p_s \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

b frame in 3D.

R_{sb} : put in columns the coord of
vectors of $\{b\}$ -frame in $\{s\}$ -frame.



$$R_{sb} = \begin{bmatrix} \sqrt{2}/2 & -\sqrt{2}/2 \\ \sqrt{2}/2 & \sqrt{2}/2 \end{bmatrix} \quad \begin{matrix} \uparrow \\ \rightarrow \end{matrix}$$

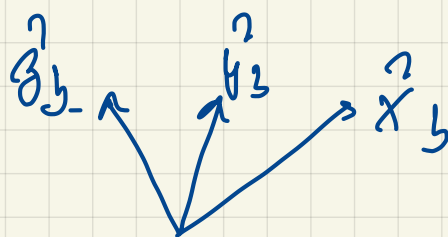
if $b = s$

$y_s = y_s$

$x_s = x_s$

$R_{sb} = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}$

3D case:



$$\|x_b^2\|^2 = 1 = x_b^2 T x_b^2$$

$$x_b^2 T y_b^2 = 0$$

$$R_{sb} = \begin{bmatrix} x_b^2 & y_b^2 & z_b^2 \end{bmatrix}$$

$$R_{sb}^T R_{sb} = \begin{bmatrix} x_b^2 T x_b^2 & x_b^2 T y_b^2 & x_b^2 T z_b^2 \\ y_b^2 T x_b^2 & y_b^2 T y_b^2 & y_b^2 T z_b^2 \\ z_b^2 T x_b^2 & z_b^2 T y_b^2 & z_b^2 T z_b^2 \end{bmatrix} \begin{bmatrix} x_b^2 & y_b^2 & z_b^2 \end{bmatrix}$$

$$= \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \quad \checkmark$$

in 2D:

$$R_{SB} = \begin{bmatrix} C_0 & -S_0 \\ S_0 & C_0 \end{bmatrix}$$

$$R_{SB}^T R_{SB} = \begin{bmatrix} C_0 & S_0 \\ -S_0 & C_0 \end{bmatrix} \begin{bmatrix} C_0 & -S_0 \\ S_0 & C_0 \end{bmatrix}$$

$$= \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}$$

$$R^T R = \mathbb{I} \quad (\Rightarrow) \quad R \text{ is an orthogonal matrix.}$$

$$\det R = ? \quad \therefore \det(R^T R) = \det(R^T)$$

$$\det(R) = 1$$

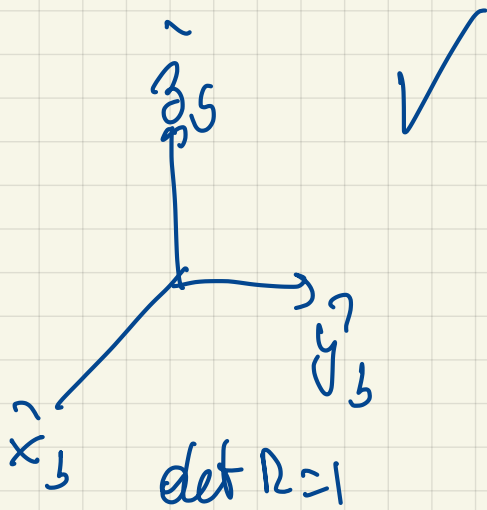
$$\leadsto [\det R]^2 = 1 \leadsto \boxed{\det R = \pm 1}$$

if $\det R = 1$ & $R^T R = I$

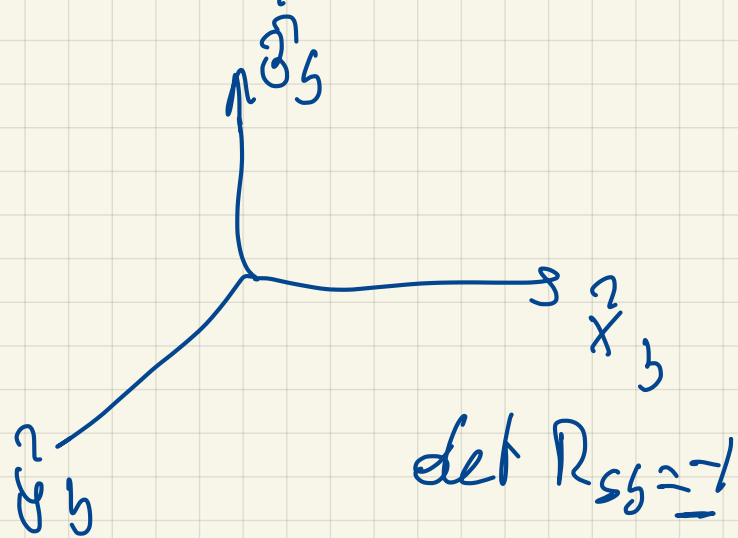
R is said to belong to the

Special orthogonal group

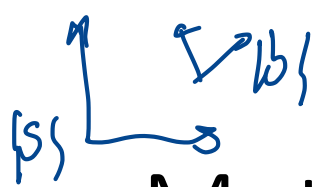
$SO(n)$



$n = 2, 3$



Rotation Matrices (2)



$$R_{aa} = I$$

$$R_{sb} = \begin{bmatrix} x_b & y_b & z_b \end{bmatrix}$$

if $b=s$

$$= \begin{bmatrix} 1 & & \\ & 1 & \\ & & 1 \end{bmatrix}$$

- We use the convention R_{ab} for the matrix whose **columns are coordinates of the frame b expressed in the frame a**
- We have the following laws:

$$R_{ab}R_{bc} = R_{ac} \text{ and } R_{ab}^{-1} = R_{ba}$$

- If the vector p_a is the vector p expressed in frame a , then

$$R_{ba}p_a = p_b$$

- If we rotate a vector v around the $\hat{\omega}$ axis by angle θ , we say $\text{Rot}(\hat{\omega}, \theta)v$

- For a rotation about the x-axis: $\text{Rot}(\hat{x}, \theta)v = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos \theta & -\sin \theta \\ 0 & \sin \theta & \cos \theta \end{bmatrix} v$

- Rotations about the y and z axis follow

Special Orthogonal Groups

$$\begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$SO(3)$, the group that represents all spatial rotation matrices, is the set of all 3×3 real matrices R that satisfy

1. $R^T R = I$

2. $\det R = 1$

- Note that (2) implies that both (1) holds and that we obey the righthand rule

Similarly, **$SO(2)$** , the group describes all planar rotation matrices, is the set of all 2×2 real matrices R , satisfying the same conditions.

• EXAM DATES have been fixed!
* EXAM 0 []

• HW2 will be posted later this week.

• Constraints.

$$\begin{cases} g_1(\theta_1, \dots, \theta_n) = 0 \\ \vdots \\ g_k(\theta_1, \dots, \theta_n) = 0 \end{cases}$$

• They are dependent if

$$\frac{\partial g}{\partial \theta} := \begin{bmatrix} \frac{\partial g_1}{\partial \theta_1} & \dots & \frac{\partial g_1}{\partial \theta_n} \\ \vdots & & \vdots \\ \frac{\partial g_k}{\partial \theta_1} & \dots & \frac{\partial g_k}{\partial \theta_n} \end{bmatrix} \text{ is of}$$

$$\text{rank } h' < h$$

$\leadsto$ they remove h' DOF.

• Non-holonomic constraints.

• Deals with velocity constraints!

• If a constraint is NON-HOLONOMIC, it does not decrease the # of DOF's.

$$\dot{\theta}_1 \theta_1 + \dot{\theta}_2 \theta_2 = 0$$

H or NH? ONLY way for argue.

H: why? It is provide g.

$\exists g$ st $\frac{d}{dt} g(\theta(t))$
 $\stackrel{!}{=} \text{constraint} = 0.$

$$g = \frac{\theta_1^2}{2} + \frac{\theta_2^2}{2} + r$$

inter

$$\frac{d}{dt} g = \frac{2\theta_1 \dot{\theta}_1}{2} + \frac{2\dot{\theta}_2 \theta_2}{2} = 0 \quad \checkmark$$

$$\dot{\theta}_1 \sin \theta_2 + \dot{\theta}_2 \sin \theta_1 = 0$$

H or NH?

try: $g = \cos \theta_2 + \cos \theta_1$

$$\frac{d}{dt} g = -\sin \theta_2 \dot{\theta}_2 - \sin \theta_1 \dot{\theta}_1 \quad \times$$

$$A = \begin{bmatrix} s_2 & s_1 \end{bmatrix} \begin{bmatrix} \dot{\theta}_1 \\ \dot{\theta}_2 \end{bmatrix} = 0$$

$s_i = \sin \theta_i$

If H, then $\exists g$ st $\frac{\partial g}{\partial \theta} = A = \begin{bmatrix} \frac{\partial g}{\partial \theta_1} & \frac{\partial g}{\partial \theta_2} \end{bmatrix}$

$\hookrightarrow \frac{\partial g}{\partial \theta_1} = s_2 \quad \frac{\partial g}{\partial \theta_2} = s_1$

$$\frac{\partial^2 g}{\partial \theta_1 \partial \theta_2} = \frac{\partial}{\partial \theta_1} \frac{\partial g}{\partial \theta_2} = \frac{\partial}{\partial \theta_1} s_1 \approx \underset{\cos \theta_1}{C_1}$$

$$\frac{\partial^2 g}{\partial \theta_2 \partial \theta_1} = \frac{\partial}{\partial \theta_2} \frac{\partial g}{\partial \theta_1} = \frac{\partial}{\partial \theta_2} s_2 = C_2$$

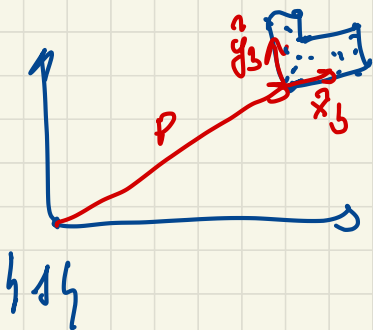
as $\mathbb{N}H$.

$$\boxed{\theta_1^2 + 3\theta_1 \cos \theta_2 = 0} \quad g!$$

$$\boxed{H} \text{ on } \mathbb{N}H? \quad \boxed{\text{no } \dot{\theta}_1 \text{ if } i \text{ is } H.}$$

$$g(\theta_1, \theta_2) = 0$$

$$; \quad \dot{\theta}_1 \theta_1 + 4\theta_1^2 + C = 0$$

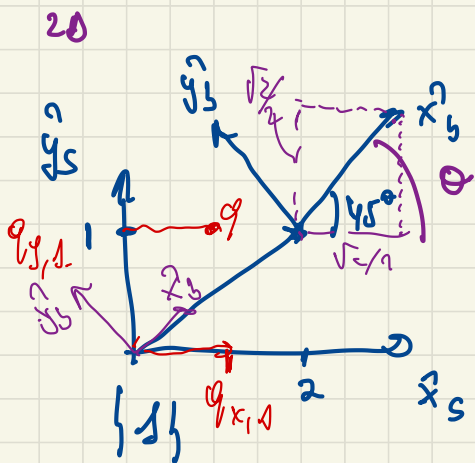


$$P = \begin{bmatrix} \hat{x}_b & \hat{y}_b \end{bmatrix}$$

$$R_{Sb} = \begin{bmatrix} \hat{x}_b & \hat{y}_b \end{bmatrix}$$

Coord
of $\hat{x}_b$ in $\{1\}$ frame

Coord of
 $\hat{y}_b$ in $\{1\}$ frame



$$P = \begin{bmatrix} 2 \\ 1 \end{bmatrix}$$

$$R_{Sb} = \begin{bmatrix} \frac{\sqrt{2}}{2} & -\frac{\sqrt{2}}{2} \\ \frac{\sqrt{2}}{2} & \frac{\sqrt{2}}{2} \end{bmatrix}$$

$$R_{Sb} = \begin{bmatrix} \cos \theta & -\sin \theta \\ \sin \theta & \cos \theta \end{bmatrix}$$

R_{Sb} = rotation matrix.

$$q = q_{x,1} \hat{x}_s + q_{y,1} \hat{y}_s$$

$$q = \begin{bmatrix} \hat{x}_s & \hat{y}_s \end{bmatrix} \begin{bmatrix} q_{x,1} \\ q_{y,1} \end{bmatrix}$$

$$\underline{q}_b = R_{b,1} \underline{q}_s$$

$$\underline{R}_{Sb} = \begin{bmatrix} \hat{x}_s & \hat{y}_s \end{bmatrix}$$

$\hookrightarrow$ coord of basis $\{1\}$ in $\{b\}$

- R_{ab} : write in columns the coord of basis $\{b\}$ in $\{a\}$

$$\left[\begin{array}{l} \text{relations:} \\ \left\{ \begin{array}{l} q_b = R_{ba} q_a \\ R_{ac} = R_{ab} R_{bc} \end{array} \right. \end{array} \right]$$

$$* R_{ab} = R_{ba}^{-1} = R_{ba}^T$$

$$R_{ab} = \begin{bmatrix} x_b & y_b & z_b \end{bmatrix} \quad R_{ab}^T = \begin{bmatrix} \overline{x_b^T} \\ \overline{y_b^T} \\ \overline{z_b^T} \end{bmatrix}$$

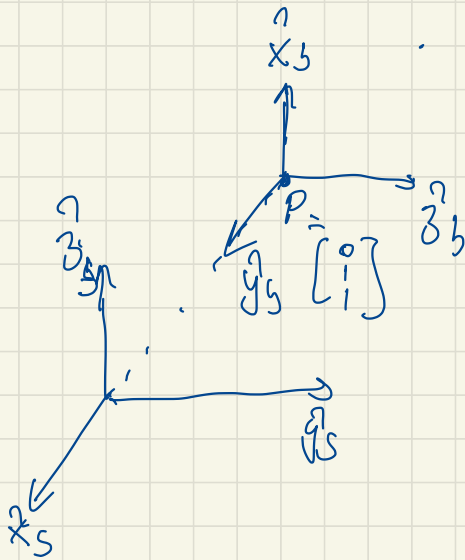
$$R_{ab}^T R_{ab} = \underline{I} \Rightarrow R_{ab}^T = R_{ab}^{-1}$$

• Frame: data of rotation & point.

$$T_{ab} = \begin{bmatrix} R_{ab} & P_a \\ 000 & 1 \end{bmatrix} : 4 \text{ by } 4 \text{ matrix in } 3D$$

$$= \begin{bmatrix} R_{ab} & P_a \\ 0 & 1 \end{bmatrix} : 3 \times 3 \text{ matrix in } 2D$$

$T_{ab} =$ R_{ab} : same as before
 (write $\{b\}$ -frame in $\{a\}$



P_e = coord of point p
 in $\{a\}$ frame.

$$T_{sb} = \begin{bmatrix} R_{sb} & P_s \\ 0 & 1 \end{bmatrix}$$

$$R_{sb} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ 1 & 0 & 0 \end{bmatrix} \quad P_s = \begin{bmatrix} 0 \\ 1 \\ 1 \end{bmatrix}$$

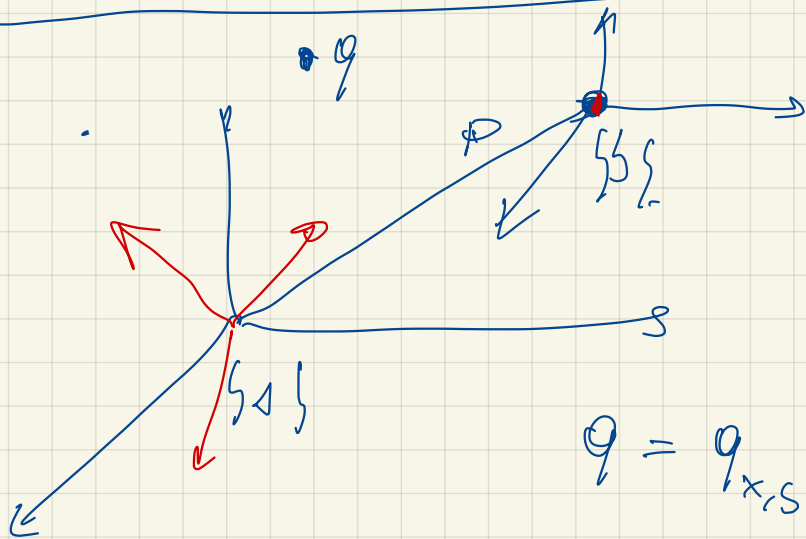
$$T_{sb}^{-1} = ?$$

$$T_{sb} T_{sb}^{-1} = I.$$

$$T_{sb}^{-1} = \begin{bmatrix} R_{sb}^T = R_{bs} & -R_{bs}P_s \\ 0 & 1 \end{bmatrix}$$

$$\begin{bmatrix} R_{sb} & P_s \\ 0 & 1 \end{bmatrix} \begin{bmatrix} R_{sb}^T & -R_{sb}^T P_s \\ 0 & 1 \end{bmatrix} = \begin{bmatrix} I & -P_s + P_s \\ 0 & 1 \end{bmatrix} = I.$$

$$T_{SS}^{-1} \neq T_{SS}^T$$



$$q = q_{x,s} \hat{x}_s + q_{y,s} \hat{y}_s + q_{z,s} \hat{z}_s$$

coord of q in $\{b\}$ frame?

$$q_s = \begin{pmatrix} q_{x,s} \\ q_{y,s} \\ q_{z,s} \\ 1 \end{pmatrix}$$

$$q_b = T_{bs} q_s$$

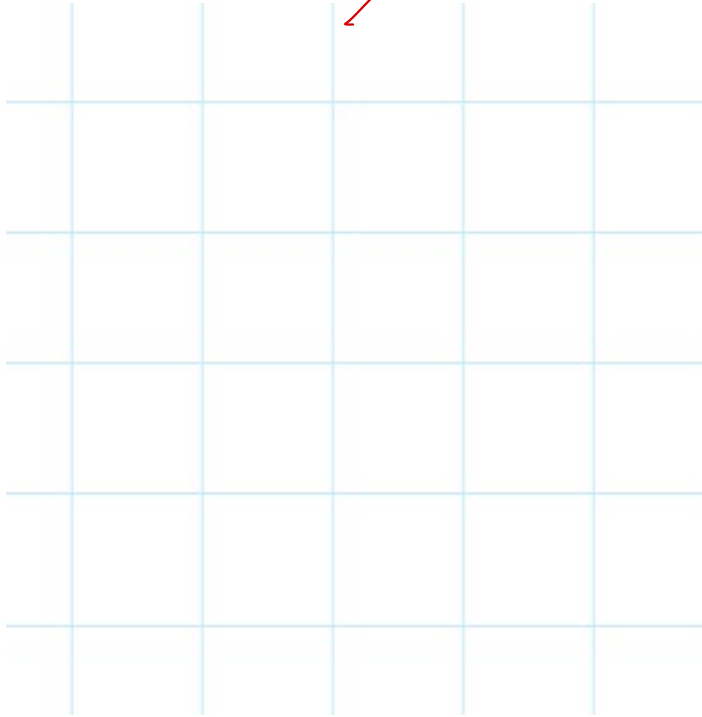
$\begin{pmatrix} q_x \\ q_y \\ q_z \\ 1 \end{pmatrix}$

$$T_{as} = \begin{bmatrix} R_{as} & p_a \\ 0 & 1 \end{bmatrix}$$

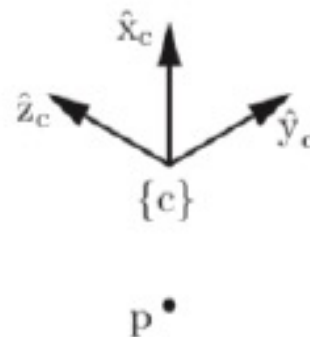
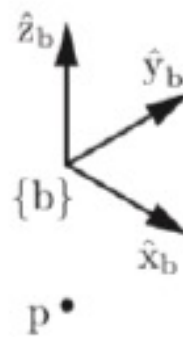
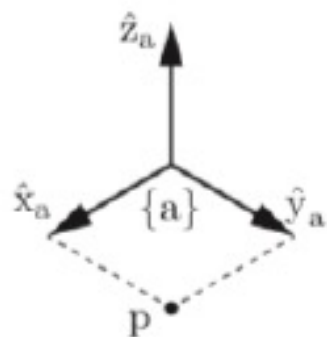
R_{as} = col. of $\{b\}$ in $\{a\}$ frame

q_a = coord of q in $\{a\}$ -frame

Changing frames



Frames in 3D

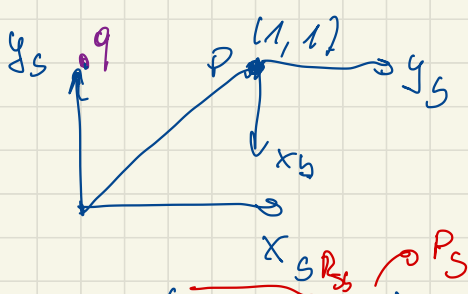


$$P_a = \begin{bmatrix} 1 \\ 1 \\ 0 \end{bmatrix}$$

$$P_b = \begin{bmatrix} 1 \\ -1 \\ 0 \end{bmatrix}$$

$$R_{ab} = \begin{bmatrix} 0 & 1 & 0 \\ 1 & 0 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$R_{ab} P_b = \begin{bmatrix} 1 \\ 1 \\ 0 \end{bmatrix} = P_a$$



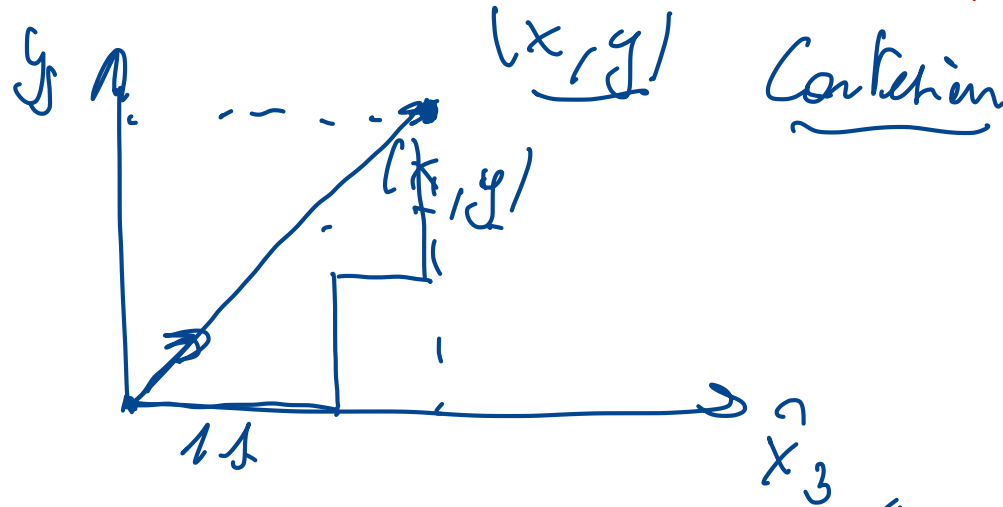
$$T_{sb} = \begin{pmatrix} 0 & 1 & 1 \\ -1 & 0 & 1 \\ 0 & 0 & 1 \end{pmatrix}$$

$$q_b = \begin{pmatrix} 0 \\ -1 \\ 1 \end{pmatrix}$$

projective coord.

$$T_{sb} q_b = \begin{pmatrix} 0 \\ -1 \\ 1 \end{pmatrix} = q_s$$

[Exponential Coordinates.]



Rigid Body Motions



Recall the cross product

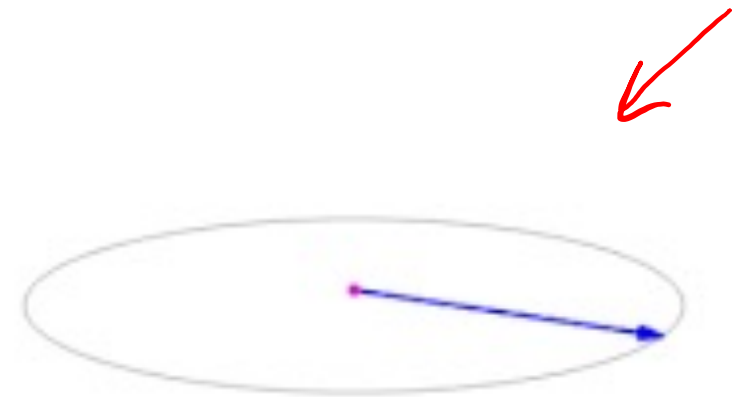
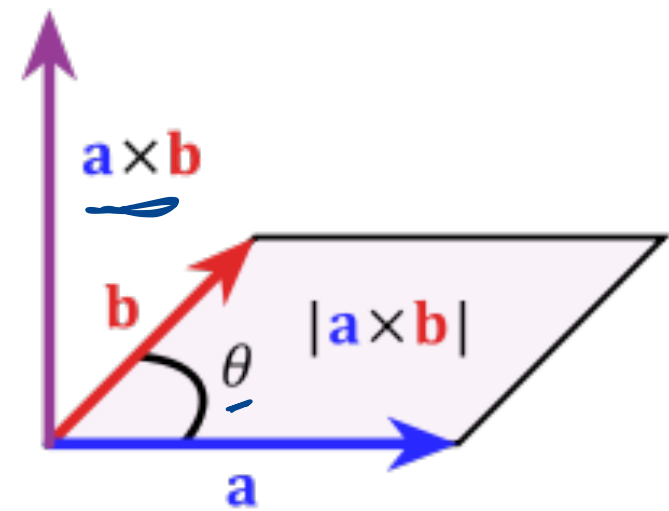
- The cross-product is defined as

$$a \times b = \|a\| \|b\| \sin \theta \hat{n}$$

- In coordinates:

$$a \times b = \begin{bmatrix} a_2 b_3 - a_3 b_2 \\ a_3 b_1 - a_1 b_3 \\ a_1 b_2 - a_2 b_1 \end{bmatrix}$$

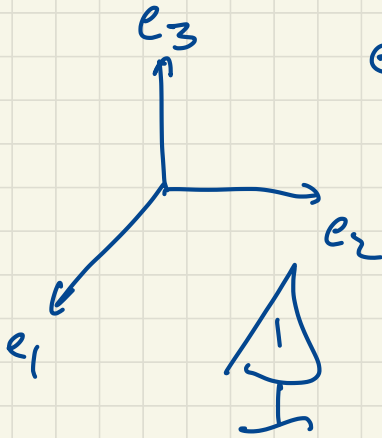
$$\begin{bmatrix} a_1 \\ a_2 \\ a_3 \end{bmatrix} \times \begin{bmatrix} b_1 \\ b_2 \\ b_3 \end{bmatrix} = \begin{bmatrix} \det \begin{bmatrix} e_2 & b_1 \\ e_3 & b_3 \end{bmatrix} \\ - \det \begin{bmatrix} e_1 & b_1 \\ e_3 & b_2 \end{bmatrix} \\ \det \begin{bmatrix} e_1 & b_1 \\ e_2 & b_2 \end{bmatrix} \end{bmatrix}$$



$$a \times b = -b \times a$$

$$\cdot \quad \underbrace{(a \times b)}_b \times \underbrace{c}_c \neq a \times \underbrace{(b \times c)}_c$$

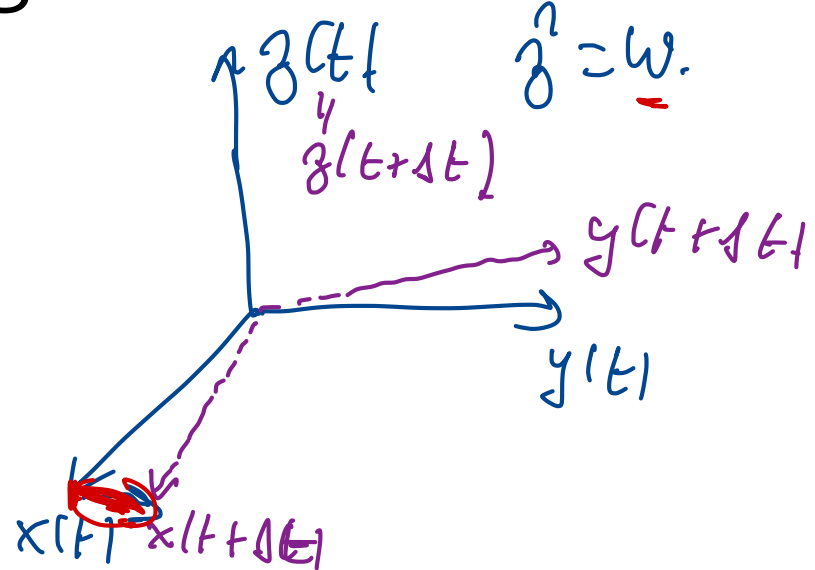
ex: $(e_1 \times e_1) \times e_2 = 0$
 $e_1 \times \underbrace{(e_1 \times e_2)}_{e_3} = e_2$



Cross product is

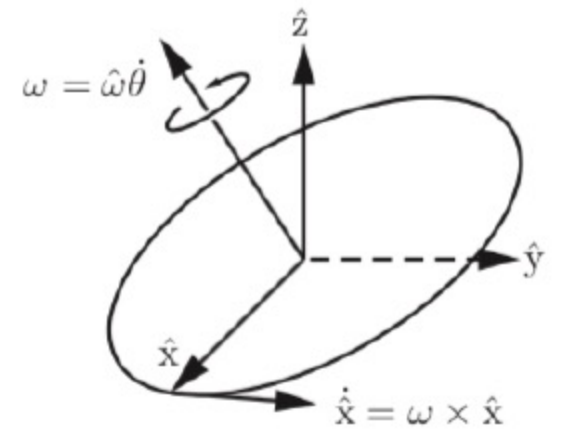
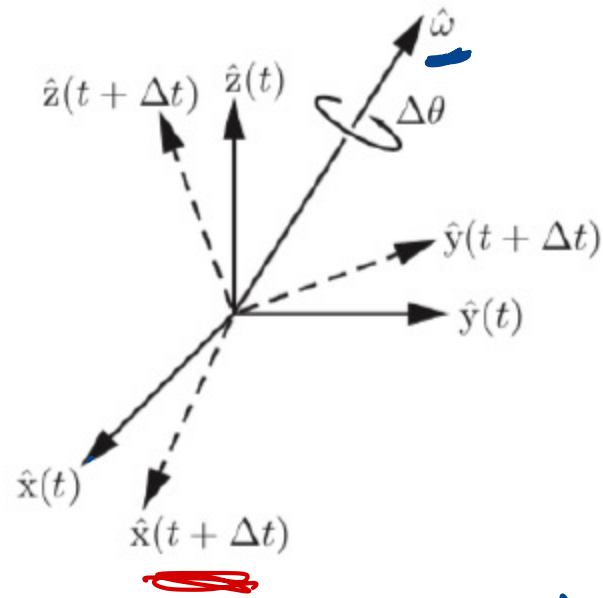
NOT associative.

Angular Velocities



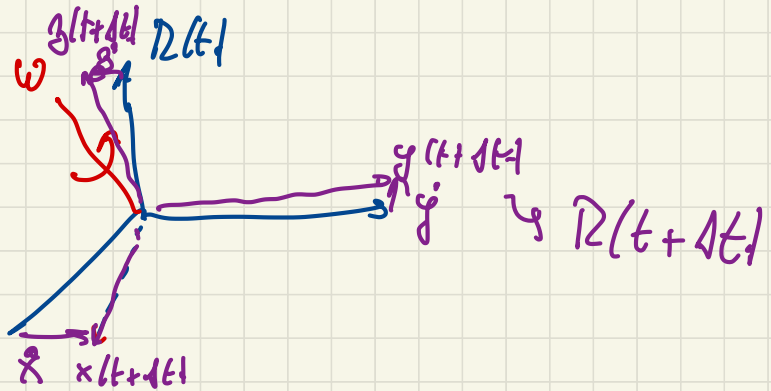
$$\underline{x}(t+\Delta t) = \underline{x}(t) + (\underline{\omega} \times \underline{x}(t)) \Delta t.$$

$$\leadsto \frac{\underline{x}(t+\Delta t) - \underline{x}(t)}{\Delta t} = \underline{\omega} \times \underline{x}(t) \leadsto \dot{\underline{x}}(t) = \underline{\omega} \times \underline{x}(t)$$



$$\frac{d}{dt} \begin{bmatrix} x(t) \\ y(t) \\ z(t) \end{bmatrix} = \underline{\omega} \times \begin{bmatrix} x(t) \\ y(t) \\ z(t) \end{bmatrix}$$

$$\frac{d}{dt} R(t) = \omega \times R(t)$$



• we don't like $\times$.

$$\omega \times x = \begin{bmatrix} \omega_2 x_3 - \omega_3 x_2 \\ \omega_3 x_1 - \omega_1 x_3 \\ \omega_1 x_2 - \omega_2 x_1 \end{bmatrix}$$

$$\begin{pmatrix} \omega_1 \\ \omega_2 \\ \omega_3 \end{pmatrix} \times \begin{pmatrix} x_1 \\ x_2 \\ x_3 \end{pmatrix}$$

$\rightarrow 3 \times 3$

Define a matrix $[w]$ st

$$[w] x = \omega \times x.$$

$$[w] = \begin{bmatrix} 0 & -\omega_3 & \omega_2 \\ \omega_3 & 0 & -\omega_1 \\ -\omega_2 & \omega_1 & 0 \end{bmatrix}$$

$$\omega = \begin{bmatrix} \omega_1 \\ \omega_2 \\ \omega_3 \end{bmatrix}$$

$$\leadsto [\omega] \doteq \begin{bmatrix} 0 & -\omega_3 & \omega_2 \\ \omega_3 & 0 & -\omega_1 \\ -\omega_2 & \omega_1 & 0 \end{bmatrix}$$

$$\rightarrow \boxed{\frac{d}{dt} R = [\omega] R} \quad \text{Rotationen}$$

$$\boxed{\frac{d}{dt} X(M) = v}$$

Translationen