Introduction to Robotics Lecture 7: Screws and wrenches

Screw motion



- 2D Screw motion: any rigid motion in the plane can be represented by a rotation around a well-chosen center.
- We can encode it with (β, s_x, s_y), where (s_x, s_y) is the position of the center of the rotation, and β the angle. Here, β = π/4 and s = (0,2)

Screw motion



- Chasles-Mozzi Theorem: Any displacement in 3D can be represented by a rotation + translation about same axis. This is called a screw motion.
- Data for a screw: Axis of rotation: q ∈ ℝ³ + ŝ ∈ S²; pitch h : ratio linear/angular speed; θ: angular velocity.
- Rotation of θ rad results in translation of $h\theta$ along axis.
- Very useful to represent motion of revolute and prismatic joints.

• Write as
$$S = \{q, \hat{s}, h\}$$
.

Ball and Chasles







 Rodrigues and Chasles took the entrance exam to Polytechnique/Normale at the same time, finishing first and second respectively. Rodrigues did not use it and elected to go to La Sorbonne.

Screw motion \rightarrow twist



- How to represent a screw motion as a twist? Take $S = \{q, \hat{s}, h\}$.
 - Rotational velocity: $\omega = \hat{s}\dot{\theta}$.
 - Linear velocity : velocity at origin of frame= translation along the screw axis + linear motion at origin induced by rotation of screw axis:

$$v = h\hat{s}\dot{ heta} - \hat{s}\dot{ heta} imes q.$$

$\mathsf{Twist} \to \mathsf{Screw} \ \mathsf{motion}$



• How to represent a twist as a screw motion? Take $\mathcal{V} = [\omega, v]^{\top}$

- ► Rotation+pitch: $\hat{s} = \omega / \|\omega\| = \bar{\omega}, \ \dot{\theta} = \|\omega\|$ and $h = \bar{\omega}^\top v / \dot{\theta} = \omega^\top v / \|\omega\|^2$.
- Offset q: Assuming ω ≠ 0 (not pure translation, so that there is a meaningful rotation axis), need to find q so that v = hŝθ − ŝθ × q. Cross product on left by ŝ yields

$$q=rac{\hat{s} imes v}{\dot{ heta}}.$$

Screw motion



For a given reference frame, we denote by S the screw axis of the screw motion {q, ŝ, θ}

$$S = \begin{bmatrix} \omega \\ \mathbf{v} \end{bmatrix}$$

with either 1: $\|\omega\| = 1$ or 2: $\omega = 0$ and $\|v\| = 1$. Case 1: then $v = -\omega \times q + h\omega$ Case 2: corresponds to a translation along v: (*h* is infinite) $\rightarrow \omega = 0$.

Exponential coordinates for Rigid-Body motions

- Recall: for a rotation R ∈ SO(3), its exponential coordinates (ω, θ) are so that R = e^{[ω]θ}. We want to do the same for rigid motions (i.e., rotation + translation)
- The matrix $[\bar{\omega}]$ was skew-symmetric: $[\bar{\omega}] \in \mathfrak{so}(3)$.
- We defined

$$\exp :\mathfrak{so}(3) \to SO(3) : A \to I + A + A^2/2! + \cdots$$
$$\log :SO(3) \to \mathfrak{so}(3) : R \to \frac{1}{2\sin\theta}(R - R^{\top})$$

Exponential coordinates for Rigid-Body motions

- ▶ By analogy, we define the exponential coordinates for a homogeneous transformation T as $S\theta \in \mathbb{R}^6$, where S is the screw axis and θ the distance around the screw axis to take a frame from I to T.
- ► Recall that if S = (ω, ν) is with ||ω|| = 1, then θ is an angle of rotation about the screw axis. If ω = 0 and ||ν|| = 1, then θ is the distance travelled along the screw axis.
- Denote by SE(3) the space of homogeneous transformations T, and by se(3) the space of their exponential coordinates. We want to define

$$\exp:\mathfrak{se}(3) \to SE(3): A \to I + A + A^2/2! + \cdots$$
$$\log:SE(3) \to \mathfrak{se}(3): T \to [S]\theta \in \mathfrak{se}(3)$$

Exponential coordinates for Rigid-Body motions For $S = [\omega, v]^{\top}$, we introduce the 4 × 4 matrix:

$$\left[\mathcal{S}
ight] := egin{bmatrix} \left[egin{smallmatrix} \omega & v \ 0 & 0 \end{bmatrix} \end{bmatrix}$$

As before, we can find a simple expression for the exponential. We have (recall: ω = ωθ)

$$e^{[\mathcal{S}]\theta} = I + [\mathcal{S}]\theta + [\mathcal{S}]^2\theta^2/2! + [\mathcal{S}]^3\theta^3/3! + \cdots$$
$$= \begin{bmatrix} e^{[\overline{\omega}]\theta} & G(\theta)v\\ 0 & 1 \end{bmatrix}$$

where $G(\theta) = I\theta + [\overline{\omega}]\theta^2/2! + [\overline{\omega}]^2\theta^3/3! + \cdots$. • Recall that $[\overline{\omega}]^3 = -[\overline{\omega}]$. We obtain

$$G(\theta) = I\theta + (\theta^2/2! - \theta^4/4! + \cdots)[\overline{\omega}] + (\theta^3/3! - \theta^5/5! + \cdots)[\overline{\omega}]^2$$

= $I\theta + (1 - \cos\theta)[\overline{\omega}] + (\theta - \sin\theta)[\overline{\omega}]^2$

Logarithm of Rigid-Body motions

• Given $T = (R, p) \in SE(3)$, we need to find $S = (\overline{\omega}, v)$ and θ so that

$$e^{[\mathcal{S}]\theta} = \begin{bmatrix} R & p \\ 0 & 1 \end{bmatrix},$$

which implies that

$$[\mathcal{S}] heta = egin{bmatrix} [\overline{\omega}] heta & extsf{v} heta\ 0 & 0 \end{bmatrix}$$

is a logarithm of T.

- ► Case 1: If R = I (pure translation), then set $\overline{\omega} = 0$, v = p/||p|| and $\theta = ||p||$.
- ▶ Case 2: 1. Obtain $\overline{\omega}, \theta$ using the matrix logarithm of *R*. 2. Set

$$v = G^{-1}(\theta)p$$

where

$$G^{-1}(heta) = rac{1}{ heta} I - rac{1}{2} [\overline{\omega}] + \left(rac{1}{ heta} - rac{1}{2}\cotrac{ heta}{2}
ight) [\overline{\omega}]^2.$$

Wrenches

- Let {a} be a ref. frame and r_a a point in a rigid body. Let the vector f_a ∈ ℝ³ represent a force acting on the body. Assume it is a point force acting at r_a.
- The force creates a *torque or moment* $m_a \in \mathbb{R}^3$ given by

$$m_a := r_a \times f_a.$$

▶ We merge the force and the moment in a single 6-dimensional vector, called *spatial force* or *wrench*, expressed in {*a*} as

$$\mathcal{F}_a := \begin{bmatrix} m_a \\ f_a \end{bmatrix}$$

- A wrench can contain only a torque and no force: it is called a *pure* moment.
- If there are several forces/moments acting on the body, we can add their corresponding wrenches.

Wrenches

- ▶ Given 2 frames, a and b, and want to express the wrench in both frames: F_a, F_b.
- Denote by V_a, V_b the motions induced by the wrench in frames a and b: we know how to relate them: V_b = Ad_{T_{ba}}V_a
- Recall: dot product of velocity and force is a power!
- Power is independent from choice of frame!

$$\begin{split} \mathcal{V}_{b}^{\top}\mathcal{F}_{b} &= \mathcal{V}_{a}^{\top}\mathcal{F}_{a} \\ &= (\operatorname{Ad}_{\mathcal{T}_{ab}}\mathcal{V}_{b})^{\top}\mathcal{F}_{a} \\ &= \mathcal{V}_{b}^{\top}(\operatorname{Ad}_{\mathcal{T}_{ab}})^{\top}\mathcal{F}_{a} \end{split}$$

• Since the previous equation holds for all \mathcal{V}_b , we have

$$\mathcal{F}_b = (\mathrm{Ad}_{\mathcal{T}_{ab}})^\top \mathcal{F}_a$$