

LECTURE 5

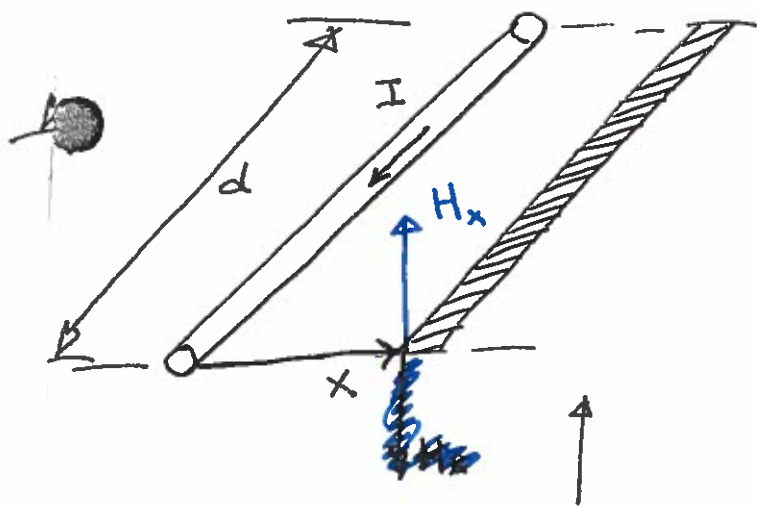
INDUCTANCE OF A SINGLE WIRE

09/12/17

- We are going to use Ampere's law to first obtain ℓ

We will start with a single infinitely long wire

- We are going to compute the flux linkages and relate to the current through the wire. Then by linearity, we will be able to obtain ℓ [H/m]



return path

@ ∞

- We will assume that the current density through the wire is uniform and the wire has a radius r .
- We will compute the flux linkages outside the wire first, and then inside the wire.

(i) Flux linkages through a surface outside the wire, infinitely long and of width R .

$$H_x 2\pi x = I \rightarrow H_x = \frac{I}{2\pi x}$$

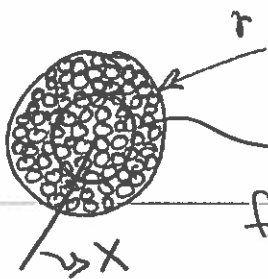
$$\begin{aligned} \Phi_1 &= \int_r^R \frac{\mu_0 I}{2\pi x} \underbrace{d \cdot dx}_{\text{differential area}} = \frac{\mu_0 d I}{2\pi} \ln \frac{R}{r} \\ &= \lambda_1 \end{aligned}$$

(ii) Flux linkage inside the conductor

$$B_2 = \mu \cdot \frac{I_2}{2\pi x} = \frac{\mu I \frac{x^2}{r^2}}{2\pi x} = \frac{\mu I x}{2\pi r^2}$$

$$\lambda_2 = \int_0^r \underbrace{\frac{\mu I x}{2\pi r^2} d \cdot dx}_{\text{diff area } d\phi} \cdot \frac{x^2}{r^2}$$

" Number of times the flux links the wire



You only link a fraction of them, x^2/r^2

$$\text{The } \lambda_2 = \int_0^r \frac{\mu I x^3}{2\pi r^4} dx = \frac{\mu I x^4}{8\pi r^4} \Big|_0^r = \frac{\mu I d}{8\pi}$$

Total flux linkages

$$\lambda = \lambda_1 + \lambda_2$$

$$= \frac{\mu_0 d I}{2\pi} \ln \frac{R}{r} + \frac{\mu I d}{8\pi} = \frac{\mu_0 d I}{2\pi} \left(\ln \frac{R}{r} + \frac{\mu r}{4} \right)$$

$$= \frac{\mu_0 d \cdot I}{2\pi} \left(\ln R - \ln r - \ln e^{-\mu r/4} \right) = \frac{\mu_0 d}{2\pi} \ln \frac{R}{r'} I$$

$$\lambda = L \cdot I \quad L = \frac{\mu_0 d}{2\pi} \ln \frac{R}{r'}$$

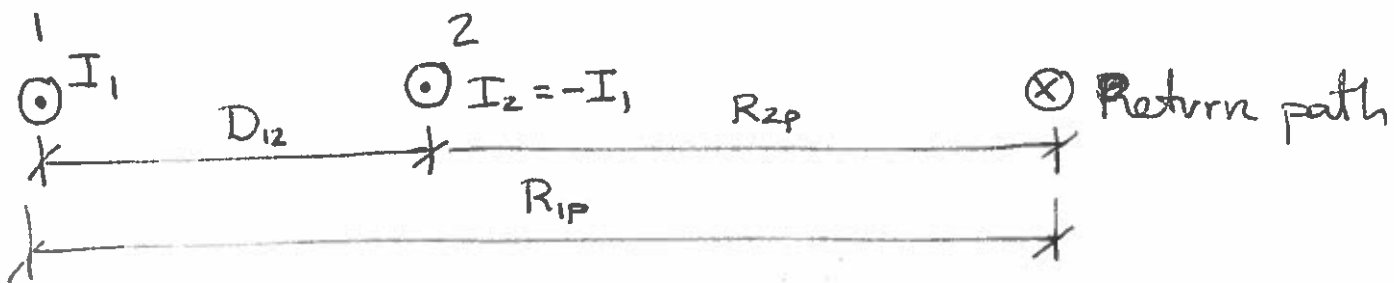
$$\boxed{\ell = \frac{L}{d} = \frac{\mu_0}{2\pi} \ln \frac{R}{r'}}$$

← This is not a finite quantity as $R \rightarrow \infty$.

We are going to use superposition now to obtain the inductance of multi-wire arrangements, namely:

- two-conductors
- three-conductors

INDUCTANCE OF A TWO-CONDUCTOR LINE



$$\lambda_1 = \lambda_{11} + \lambda_{12}$$

$$\lambda_{11} = \frac{\mu_0 d}{2\pi} \ln \frac{R_{1P}}{r'} \cdot I_1 \quad \leftarrow \text{flux linked by conductor 1 due to } I_1$$

$$\lambda_{12} = \frac{\mu_0 d}{2\pi} \ln \frac{R_{2P}}{D_{12}} I_2 \quad \leftarrow \text{flux linked by conductor 1 due to } I_2$$

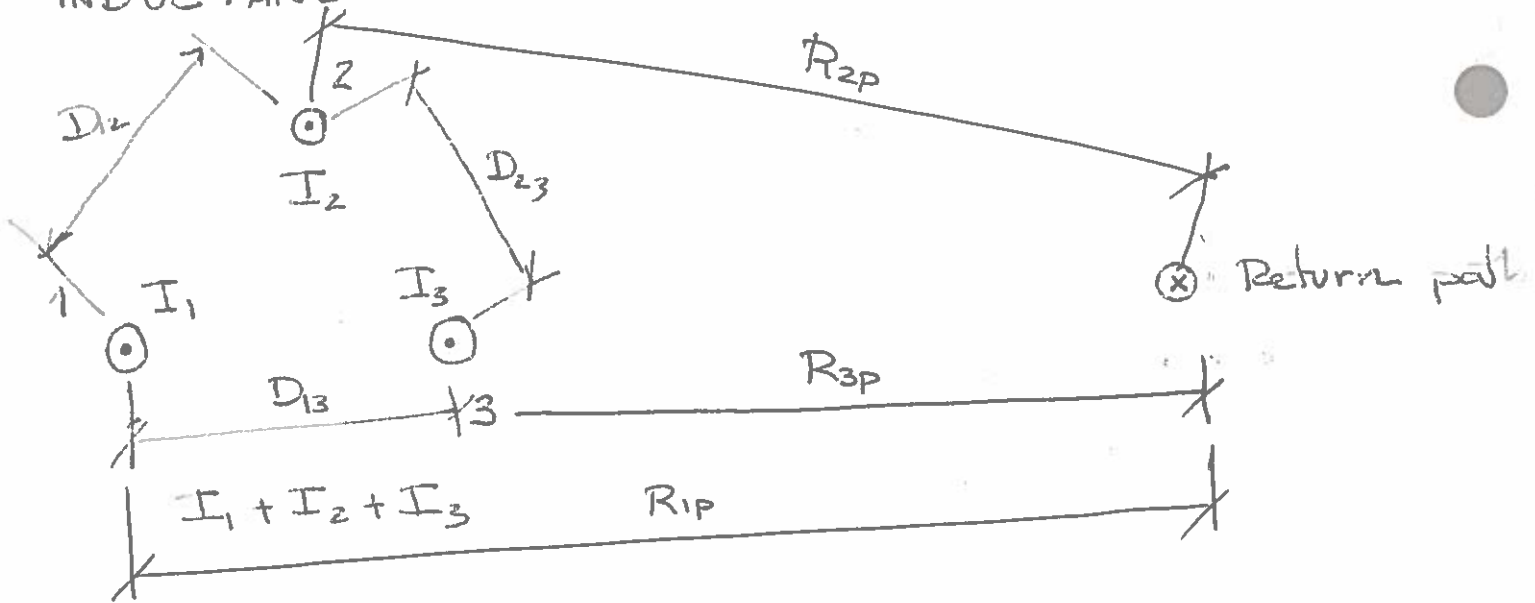
$$\lambda_1 = \frac{\mu_0 d}{2\pi} \left[\ln \frac{R_{1P}}{r'} - \ln \frac{R_{1P} - D_{12}}{D_{12}} \right] I_1$$

$$= \frac{\mu_0 d}{2\pi} \left[\ln \frac{D_{12}}{r'} + \ln \frac{R_{1P}}{R_{1P} - D_{12}} \right] I_1 \quad \text{as } R_{1P} \rightarrow \infty$$

$$L := \frac{\mu_0 d}{2\pi} \ln \frac{D_{12}}{r'}$$

$$l = \frac{\mu_0 d}{2\pi} \ln \frac{D_{12}}{r'}$$

INDUCTANCE OF A THREE-CONDUCTOR LINE



$$\lambda_1 = \lambda_{11} + \lambda_{12} + \lambda_{13}$$

$$\lambda_{11} = \frac{\mu_0 d}{2\pi} L_n \frac{R_{1p}}{r_1} \cdot I_1$$

$$\lambda_{12} = \frac{\mu_0 d}{2\pi} L_n \frac{R_{2p}}{D_{12}} I_2$$

$$\lambda_{13} = \frac{\mu_0 d}{2\pi} L_n \frac{R_{3p}}{D_{13}} I_3$$

Coupling with other phase

$$\lambda_1 = \frac{\mu_0 d}{2\pi} \left[L_n \frac{1}{r_1} I_1 + L_n \frac{1}{D_{12}} I_2 + L_n \frac{1}{D_{13}} I_3 + L_n R_{1p} I_1 + L_n R_{2p} I_2 + L_n R_{3p} I_3 \right]$$

$$D = D_{12} = D_{13}, \quad I_2 + I_3 = -I_1, \quad R_{1p} = R_{2p} = R_{3p} = R_p$$

$$\downarrow$$

$$= \frac{\mu_0 d}{2\pi} \left[L_n \frac{D}{r_1} I_1 + L_n R_p \cdot (I_1 + I_2 + I_3) \right]$$

$$\lambda = \frac{\mu_0 d}{2\pi} L_n \frac{D}{r_1} I_1$$

$$C = \frac{\epsilon_0}{2\pi} L_n \frac{D}{r_1}$$

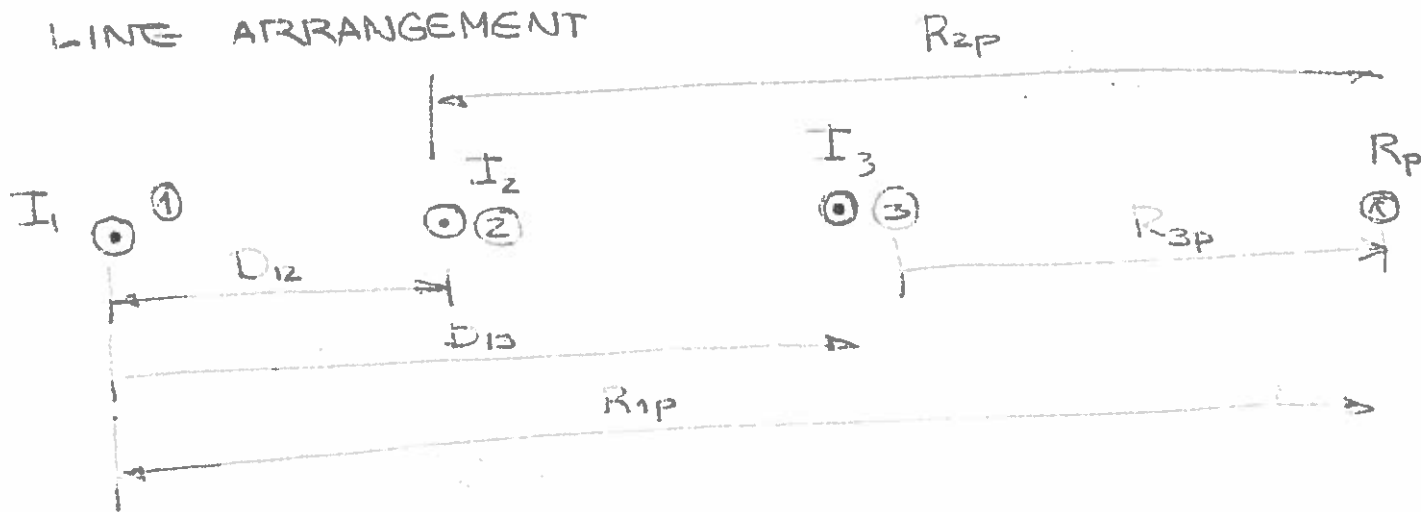
$$\lambda_1 = \frac{\mu_0 d}{2\pi} \ln \frac{D}{r'} I_1$$

$$l = \frac{\mu_0}{2\pi} \ln \frac{D}{r'}$$

Even if there was coupling between the phases, in a symmetric configuration, the magnetic coupling can be modeled using self-inductances: GOOD!

INDUCTANCE OF A THREE CONDUCTOR:

LINE ARRANGEMENT



$$\lambda_1 = \lambda_{11} + \lambda_{12} + \lambda_{13}$$

$$\lambda_1 = \frac{\mu_0 d}{2\pi} \ln \frac{R_{1p}}{r'} I_1$$

$$\lambda_2 = \frac{\mu_0 d}{2\pi} \ln \frac{R_{2p}}{D_{12}} I_2$$

$$\lambda_3 = \frac{\mu_0 d}{2\pi} \ln \frac{R_{3p}}{D_{13}} I_3$$

$$\lambda_1 = \frac{N_{od}}{2\pi} \left(\text{Ln} \frac{R_{1p}}{r'} I_1 + \text{Ln} \frac{R_{2p}}{D_{12}} I_2 + \text{Ln} \frac{R_{3p}}{D_{13}} I_3 \right)$$

$$= \frac{N_{od}}{2\pi} \left(\text{Ln} \frac{1}{r'} I_1 + \text{Ln} \frac{1}{D_{12}} I_2 + \text{Ln} \frac{1}{D_{13}} I_3 + I_1 \text{Ln} R_{1p} + I_2 \text{Ln} R_{2p} + I_3 \text{Ln} R_{3p} \right)$$

$$= \frac{N_{od}}{2\pi} \left(\text{Ln} \frac{1}{r'} I_1 + \text{Ln} \frac{1}{D_{12}} I_2 + \text{Ln} \frac{1}{D_{13}} I_3 \right)$$

$$+ \frac{N_{od}}{2\pi} \left(\text{Ln} R_p (I_1 + I_2 + I_3) \right)$$

$$\lambda_1 = \frac{N_{od}}{2\pi} \left(\text{Ln} \frac{1}{r'} I_1 + \text{Ln} \frac{1}{D_{12}} I_2 + \text{Ln} \frac{1}{D_{13}} I_3 \right)$$

$$L_{11} = \frac{N_0}{2\pi} \text{Ln} r'$$

$$L_{12} = \frac{N_0}{2\pi} \text{Ln} \frac{1}{D_{12}}$$

$$L_{13} = \frac{N_0}{2\pi} \text{Ln} \frac{1}{D_{13}}$$

There is magnetic coupling between the phases!

$$\lambda_1 = \frac{N_{od}}{2\pi} \left(\text{Ln} \frac{1}{r'} I_1 + \text{Ln} \frac{1}{D_{12}} I_2 + \text{Ln} \frac{1}{D_{13}} I_3 \right)$$

$$\lambda_2 = \frac{N_{od}}{2\pi} \left(\text{Ln} \frac{1}{r'} I_2 + \text{Ln} \frac{1}{D_{12}} I_1 + \text{Ln} \frac{1}{D_{23}} I_3 \right)$$

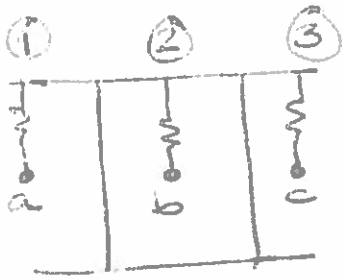
$$\lambda_3 = \frac{N_{od}}{2\pi} \left(\text{Ln} \frac{1}{r'} I_3 + \text{Ln} \frac{1}{D_{23}} I_2 + \text{Ln} \frac{1}{D_{13}} I_1 \right)$$

$$I_1 + I_2 + I_3 = 0$$

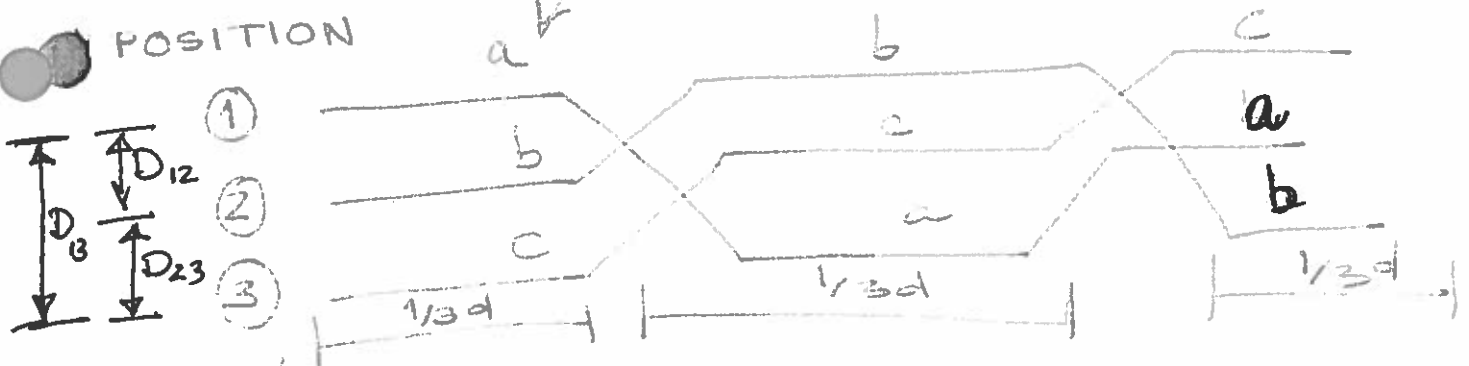
TRANSPOSITION

To keep the system balanced over the length of a transmission line, the conductors are rotated so each phase occupies each position of the tower for an equal distance.

This is known as TRANSPOSITION



POSITION



Flux linkages:

$$\lambda_a = \frac{1}{3} \frac{V_0 d}{2\pi} \left[I_a \ln \frac{1}{r} + I_b \ln \frac{1}{D_{12}} + I_c \ln \frac{1}{D_{13}} \right]$$

$$+ \frac{1}{3} \frac{V_0 d}{2\pi} \left[I_a \ln \frac{1}{r} + I_b \ln \frac{1}{D_{13}} + I_c \ln \frac{1}{D_{23}} \right]$$

$$+ \frac{1}{3} \frac{V_0 d}{2\pi} \left[I_a \ln \frac{1}{r} + I_b \ln \frac{1}{D_{23}} + I_c \ln \frac{1}{D_{12}} \right]$$

$$= \frac{V_0 d}{2\pi} \left[I_a \ln \frac{1}{r} + \ln \frac{1}{\sqrt{D_{12} D_{13} D_{23}}} (I_b + I_c) \right]$$

$$= \frac{V_0 d}{2\pi} \left[I_a \ln \frac{1}{r} + \ln \frac{1}{\sqrt{D_{12} D_{13} D_{23}}} (I_b + I_c) - I_a \right]$$

$$\lambda_a = \frac{N_0 d}{2\pi} \ln \frac{\sqrt[3]{D_{12} D_{13} D_{23}}}{r'}$$

$$l_a = \frac{N_0}{2\pi} \ln \frac{D_m}{r'}$$

$D_m = \sqrt[3]{D_{12} D_{13} D_{23}}$ is the geometric mean distance between physical positions.

GAUSS' LAW

- Similar to Ampere's law for magnetic fields, Gauss' law allows us to compute ~~electric~~ electric fields created by charges.
- In integral form

$$\oint_S \underline{D} \cdot \underline{E} d\vec{a} = Q$$

\underline{E} : Electric field intensity [V/m]

\underline{D} : Electric flux density [C/m²]

ϵ : Permittivity [F/m]

Q : Charge enclosed by the closed surface S [C]